5641

Form 504
Rev. Dec. 1933
DEPARTMENT OF COMMERCE
U.S. COAST AND GEODETIC SURVEY
R. S. PATTON, DIRECTOR

DESCRIPTIVE REPORT

AIR PHOTO

FIELD 8

Topographic } *Sheet No* REG. 5641
~~Hydrographic~~ }

State NEW JERSEY

LOCALITY

~~ATLANTIC COUNTY~~

GREAT EGG RIVER

~~JOB POINT TO GIBSON LANDING~~

Middle River

1936

CHIEF OF PARTY

E. H. Kirsch

U.S. GOVERNMENT PRINTING OFFICE: 1936

5641

1216-#1

Applied to drawing of Chart 1217 - May 5, 1938 - JTW

Supplemental " " " " " " June 16, " JTW

" " compilation of new nine Chart 827 July 6, 1939 BR.

Form 537a
Ed. Nov. 1929

DEPARTMENT OF COMMERCE
U.S. COAST AND GEODETIC SURVEY

REG. NO.

TOPOGRAPHIC TITLE SHEET

The Topographic Sheet should be accompanied by this form, filled in as completely as possible, when the sheet is forwarded to the Office.

Field No. 8

REGISTER NO. 5641 T5641

State NEW JERSEY

General locality GREAT EGG RIVER

Locality ~~JOB POINT TO GIBSON LANDING~~ Middle River
Photographs 4-22-32

Scale 1:10 000 Date of survey Compilation April 19 36

Vessel Air Photo Party No. 21.

Chief of party E. H. Kirsch

Surveyed by See data sheet in descriptive report

Inked by W. W. King

Heights in feet above --- to ground to tops of trees

Contour, Approximate contour, Form line interval --- feet

Instructions dated May 16th, 1935, 19

Remarks: NONE

SHEET NO. 8

REG. NO. 5641

PHOTO NOS.		DATES
66-52	4 to 6	7-30-32
66-13	73 to 76	4-22-32
66-13	77 to 80	4-22-32
66-14	19A to 21	4-22-32
66-8	18 to 19	4-18-32

PROJECTION MADE BY L. C. RIPLEY 4-29-35

PROJECTION CHECKED BY T. B. NUTTING 4-29-35

CONTROL PLOTTED BY J. C. SAMMONS JAN. 1936

CONTROL CHECKED BY W. W. KING Apr. 1936

CONTROL ON PHOTOS BY J. C. SAMMONS FEB. 1936

CONTROL CHECKED ON PHOTOS BY W. W. KING APR. 1936

SMOOTH RADIAL PLOT BY J. C. SAMMONS MAR. 1936

SMOOTH RADIAL PLOT CHECKED BY E. H. Kirsch E. H. KIRSCH MAR. 1936

DETAIL INKED BY W. W. KING MAR. & APR. 1936

All of the above men have been discharged or transferred.
E.H.K.

DETAIL INKED: 26 square statute miles

LENGTH OF COAST LINE: none

LENGTH OF SHORE LINE: 17.5 statute miles (more than 200 meters wide)

LENGTH OF STREAMS: 40 statute miles(Less than 200 meters wide)

Ref. Sta. Jeff, 1935 39° 19' 02.922 (90.1 m)
74° 39' 05.470 (131.0 m)

N.J. Grid x = 2,004,285.64 ft.
y = 176,931.67 ft.

DEACRIPTIVE REPORT FOR SHEET FIELD NO. 8

REGISTER NO. T5641

GENERAL INFORMATION

STATISTICS:

This sheet covers a land area of 26 square statute miles. There are 17.5 statute miles of shore line more than 200 meters wide, and 40 statute miles of streams less than 200 meters in width. There is no coast line on this sheet.

GENERAL REPORT:

This sheet includes the lower portion of the Great Egg River from Job Point to Gibson Landing. The River is bounded on both sides by large areas of low marsh land,(locally called medows) drained by numerous small ditches dug by the N. J. mosiquito and Pest control. The marsh,(partly salt and partly fresh) grows very profusely in these areas and sometimes reaches a height of 5 or 6 feet. These low areas are interspersed with many small streams winding their way to the larger ones. The vegetation appears to have been burned over and there now is a dense growth of brush, scrub oak and pine. It was learned from field inspection that in the vicinity of triangulation station GIBSON the land contains a rich deposit of charcoal as a result of this burning.

PHOTOGRAPHS:

This sheet is compiled from parts of five flights of single lens 1:10 000 scale, aerial photographs, taken by the Aero Service Corp. of Philadelphia, Penn. The flights of these photographs run approximately north and south. The time of the day at which they were taken is not available.

The Photographs used for the compilation of this sheet and their dates are as follows:

PHOTOGRAPHS NUMBERS	DATES
66-52- 4 to 6	7-30-32
66-13- 73 to 76	4-22-32
66-13- 77 to 80	4-22-32
66-14- 19A to 21	4-22-32
66-8- 18 to 19	4-18-32

Most of these photographs are clear as to detail, but some have excessive distortion. This will be further discussed in the paragraph on radial plot.

CONTROL

SOURCES:

Triangulation by Lieut. Benjamin H, Rigg, 1935. Triangulation

by Lieut. John Bowie Jr. 1935. N. J. Geod. S. Nos. 1863, 1864, 1867 and 1868, by The N. J. Geod Control Survey. All control is on N. A. 1927 datum. No graphic control sheets have been started in this area, and none will be started in the 1936season. An eleven mile traverse was run by the photo party. The computations are submitted with this report. The only marked station located by this traverse is N. J. Geod S. No. 1896. Stations 1897, 1898 and 1899 were located by pictures controlled by the traverse.

ERRORS:

No plottable errors were found in the control. The closing error of the traverse was 1.5 meters. No adjustment was made.

COMPILATION

METHOD:

The usual radial line method as described in "Notes on the compilation of planimetric line maps from 5 lens aerial photographs" was used in compiling this sheet.

ADJUSTMENTS OF THE PLOT:

The plot on this sheet was quite troublesome. Part of the trouble is due to many short flights, and partly because the plot was done in the winter months with a very low office humidity. It was after this trouble was encountered that the traverse was run. The traverse and existing triangulation gave rigid control over the entire sheet. We then attempted to raise the humidity in the office and still had trouble. Templates were then made for all pictures on the sheet, and the best possible adjustment was made with the templates. We were still troubled with two sets of cuts, from two flights, on the same point. The maximum difference between any two sets of cuts was 7 to 8 meters. A mean of all cuts was accepted for the position of the radial point, so the plot should be accurate to within 4 or 5 meters.

INTERPRETATION:

There was no difficulty in interpreting the photos. All photos were quite clear.

INFORMATION FROM OTHER SOURCES:

Control stations 1863, 1864, 1867 and 1868 from N. J. Geod Control Survey. Names from a map published by the N. J. Dept. of Conservation and Development.

CONFLICTING NAMES:

All names used were taken from U. S. C. & G. S. Chart No. 1217 and from the N. J. map referred to above. The N. J. Map by the Dept. of Conservation and Development,* calls the principle river on the sheet, GREAT EGG HARBOR RIVER. The GREAT EGG RIVER has been used on the overlay which is in accordance with chart 1217.

Jeffries Landing - Chart 8 overlay — Jeffers Landing N.J. Map.

* Sheet 36 on file in Geog. Names.

COMPARISON WITH OTHER SURVEYS

JUNCTIONS:

Satisfactory junctions have been made with sheet 5640 on the north, with sheet 5639 on the east, and 5642 and 5643 on the south. The western edge of this sheet is the limit of compilations.

LANDMARKS:

A list of recoverable stations, form 524, is submitted with this report. Landmarks for charts will be submitted as a separate report for the projeet at the end of the season.

BRIDGES:

NONE.

RECOMMENDATIONS FOR FURTHER SURVEYS:

This compilation is believed to have a probable error of not more than .7 MM in position of any detail. The sheet is complete in all detail of importance for charting. In case of a descrepency between the position of shore line on this sheetand any future graphic control sheet or hydrographic sheet, this sheet should give way for reasons discussed in the paragraph "ADJUSTMENTS OF PLOT".

Submitted by E. H. Kirsch.

E. H. Kirsch

DEPARTMENT OF COMMERCE
U. S. COAST AND GEODETIC SURVEY
Form 27
Ed. April, 1929

POSITION COMPUTATION, THIRD-ORDER TRIANGULATION

			°	′	″
α	2 Jeff	to 3 Azimuth mark	182	39	24.1
2d ∠		&	+		
α	2 "	to 1 "	182	39	24.1
Δα				+	.5
			180	00	00.0
α′	1 Az M	to 2 Jeff	2	39	24.6

			°	′	″
α	3 Az. M	to 2 Jeff	2	39	24.6
3d ∠		&	+193	20	03.5
α	3 Az M	to 1 T.P.1	195	59	28.1
Δα				+	1.7
			180	00	00.0
α′	1 T.P.1	to 3 Az. M.	15	59	29.8

First Angle of Triangle

	°	′	″			°	′	″
φ	39	19	02.922	2 Jeff	λ	74	39	05.470
Δφ		+	12.948	399.73	Δλ		−	.773
φ′	39	19	15.870	1 Az. mark	λ′	74	39	04.697

	°	′	″			°	′	″
φ	39	19	15.870	3 Az m.	λ	74	39	04.697
Δφ		+	7.144	229.19	Δλ			−2.636
φ′	39	19	23.014	1 T.P.1	λ′	74	39	02.061

	Logarithms	Values in seconds
s	2.601767	489.4 (1361.0) 1850.0
Cos α	9.999533	
B	8.510904	
h	1.112204	1st term 12.948
s²	5.203553	
Sin²α	7.332112	
C	1.31786	
	3.853351	2d term +
h²	22	
D	2.3837	
	4.60	3d term +
		−Δφ −12.948

	°	′	″
½(φ+φ′)	39	19	09.4

	Logarithms	Values in seconds
s	2.601767	112.5 (1324.8) 1437.3
Sin α	8.666059	
A′	8.509136	
Sec φ′	0.111480	
Δλ	9.888442	.77346
Sin ½(φ+φ′)	9.801843	
−Δα	9.690285	−.49010

	Logarithms	Values in seconds
s	2.360196	709.7 (1140.6) 1850.3
Cos α	9.982861	
B	8.510903	
h	0.853960	1st term 7.1443
s²	4.720392	
Sin²α	8.880202	
C	1.31792	
	4.918514	2d term +
h²	1 7179	
D	2.3837	
		3d term +
		−Δφ −7.144

	°	′	″
½(φ+φ′)	39	19	19.4

	Logarithms	Values in seconds
s	2.360196	49.4 (1387.9) 1437.3
Sin α	9.440104	
A′	8.509136	
Sec φ′	0.111492	
Δλ	0.420928	2.6359
Sin ½(φ+φ′)	9.801869	
−Δα	0.222797	.16703

11—9362 U. S. GOVERNMENT PRINTING OFFICE: 1929

DEPARTMENT OF COMMERCE
U. S. COAST AND GEODETIC SURVEY
Form 27
Ed. April, 1929

POSITION COMPUTATION, THIRD-ORDER TRIANGULATION

			°	′	″
α	2 T.P.1 to 3 Az. M.		15	59	29.8
2d ∠	&		+186	18	40.0
α	2 T.P.1 to 1 T.P.2		202	18	09.8
Δα				+	12.1
			180	00	00.0
α′	1 T.P.2 to 2 T.P.1		22	18	21.9

			°	′	″
α	3 T.P.2 to 2 T.P.1		22	18	21.9
3d ∠	&		+191	41	50.9
α	3 T.P.2 to 1 T.P.3		214	00	12.8
Δα				+	4.5
			180	00	00.0
α′	1 T.P.3 to 3 T.P.2		34	00	17.3

First Angle of Triangle

	°	′	″			°	′	″
φ	39	19	23.014	2 T.P.1	λ	74	39	02.061
Δφ		+	36.093	1203.08 ✓	Δλ		−	19.063
φ′	39	19	59.107	1 T.P.2	λ′	74	38	42.998

	°	′	″			°	′	″
φ	39	19	59.107	3 T.P.2	λ	74	38	42.998
Δφ		+	8.128	302.36	Δλ		−	7.060
φ′	39	20	07.235	1 T.P.3	λ′	74	38	35.938

	Logarithms	Values in seconds
s	3.080295	1822.83 − (27 53) / 1850.36
Cos α	9.966 232	
B	8.510 902	
h	1.537430	1st term 36.″0936
s²	6.16059	
Sin² α	9.15842	
C	1.31796	
	6.63697	2d term + .0004
h²	3.1148	
D	2.3837	
	5.4985	3d term + ~
		−Δφ −36.093

	°	′	″	Logarithms	Values in seconds
½(φ+φ′)	39	19	41.06		
s				3.080295	−1029.8 (407.2) / 1437.0
Sin α				9.579 212	
A′				8.509 136	
Sec φ′				0.111 554	
Δλ				1.280197	190.″633
Sin ½(φ+φ′)				9.801 925	
−Δα				1.082 122	+12.081

	Logarithms	Values in seconds
s	2.480524	223.1 − (16 27.3) / 1855.04
Cos α	9.918 555	
B	8.510 902	
h	0.909 981	1st term 8.″129
s²	4.96104	
Sin² α	9.49520	
C	1.318 11	
	5.77435	2d term + ~
h²	1.8200	
D	2.3838	
	~	3d term + ~
		−Δφ −8.128

	°	′	″	Logarithms	Values in seconds
½(φ+φ′)	39	20	03.1		
s				2.480524	860.71 − (576.3) / 1437.0
Sin α				9.747 602	
A′				8.509 135	
Sec φ′				0.111 568	
Δλ				0.848 829	70.″604
Sin ½(φ+φ′)				9.801 981	
−Δα				0.650 410	+4.475

11—9362 U. S. GOVERNMENT PRINTING OFFICE. 1929

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U. S. COAST AND GEODETIC SURVEY
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Ed. April, 1929

POSITION COMPUTATION, THIRD-ORDER TRIANGULATION

			°	′	″
α	2 T.P.3	to 3 T.P.2	34	00	17.3
2d ∠		&	+195	48	32.1
α	2 T.P.3	to 1 T.P.4	229	48	49.4
Δα				+	10.0
			180	00	00.0
α′	1 T.P.4	to 2 T.P.3	49	48	59.4

			°	′	″
α	3 TP4	to 2 T.P.3	49	48	59.4
3d ∠		&	-171	04	24.2
α	3 T.P.4	to 1 T.P.5	220	53	23.6
Δα				+	11.6
			180	00	00.0
α′	1 T.P.5	to 3 T.P.4	40	53	35.2

First Angle of Triangle

	°	′	″			°	′	″
φ	39	20	07.235	2 T.P.3	λ	74	38	35.938
Δφ		+	10.378	496.00	Δλ		−	15.822
φ′	39	20	17.613	1 T.P.4	λ′	74	38	20.116

	°	′	″			°	′	″
φ	39	20	17.613	3 T.P.4	λ	74	38	20.116
Δφ		+	16.417	669.71	Δλ		−	18.307
φ′	39	20	34.030	1 T.P.5	λ′	74	38	01.809

	Logarithms	Values in seconds
s	2.695482	543.18
Cos α	9.809745	(1307.20)
B	8.510902	1850.38
h	1.016129	1st term 10.3784
s²	5.390962	
Sin²α	9.766133	
C	1.318131	
	6.475226	2d term +.0003
h²	0.032257	
D	2.383838	
	~	3d term + ~
		−Δφ +10.378

	°	′	″
½(φ+φ′)	39-20-12.4		
	Logarithms	Values in seconds
s	2.695482	481.77
Sin α	9.883065	(955.22)
A′	8.509135	1436.99
Sec φ′	0.111586	
Δλ	1.199768	15.8223
Sin½(φ+φ′)	9.802005	
−Δα	1.001773	+10.029

	Logarithms	Values in seconds
s	2.825887	1049.47
Cos α	9.878504	(800.9)
B	8.510902	1850.37
h	1.215293	1st term 16.4170
s²	5.651774	
Sin²α	9.631956	
C	1.318154	
	6.601884	2d term +.0004
h²	0.004306	
D	2.477	
	~	3d term + ~
		−Δφ −16.417

	°	′	″
½(φ+φ′)	39-20-25.8		
	Logarithms	Values in seconds
s	2.825887	−43.34
Sin α	9.815981	(1393.47)
A′	8.509135	1434.81
Sec φ′	0.111614	
Δλ	1.262617	18.307
Sin½(φ+φ′)	9.802040	
−Δα	1.064657	−11.605
	1.064657	

11—9362 U. S. GOVERNMENT PRINTING OFFICE. 1929

DEPARTMENT OF COMMERCE
U. S. COAST AND GEODETIC SURVEY
Form 27
Ed. April, 1929

POSITION COMPUTATION, THIRD-ORDER TRIANGULATION

			°	'	"
α	2 T.P.5	to 3 T.P.4	40	53	35.2
2d ∠		&	+166	25	40.0
α	2 T.P.5	to 1 T.P.6	207	19	15.2
Δα				+	20.4
			180	00	00.0
α'	1 T.P.6	to 2 T.P.5	27	19	35.6

			°	'	"
α	3 T.P.6	to 2 T.P.5	27	19	35.6
3d ∠		&	+181	20	21.7
α	3 T.P.6	to 1 T.P.7	208	39	57.3
Δα				+	10.2
			180	00	00.0
α'	1 T.P.7	to 3 T.P.6	28	40	07.5

First Angle of Triangle

	°	'	"		λ	°	'	"
φ	39	20	34.030	2 T.P.5	λ	74	38	01.809
Δφ		+	48.278	1675.8	Δλ		−	32.125
φ'	39	21	22.308	1 T.P.6	λ'	74	37	29.684

	°	'	"		λ	°	'	"
φ	39	21	22.308	3 T.P.6	λ	74	37	29.684
Δφ		+	22.810	801.7	Δλ		−	16.064
φ'	39	21	45.118	1 T.P.7	λ'	74	37	13.620

	Logarithms	Values in seconds
s	3.224227	1688.0
Cos α	9.948633	(1162.4)
B	8.510902	1504
h	1.683762	1st term 48.2794
s²	6.448454	
Sin² α	9.372357	
C	1.31824	
	7.09026	2d term +.0012
h²	3.36757	
D	2.38328	
	5.7	3d term + ~
		−Δφ 48.278

	°	'	"	Values in seconds
½(φ+φ')	39	20	58.1	
	Logarithms			
s	3.224227			710.8
Sin α	9.661787			(725.8)
A'	8.509135			1436
Sec φ'	0.111698			
Δλ	1.506847			32.125
Sin ½(φ+φ')	9.802123			
−Δα	1.308950			+20.368
				970

	Logarithms	Values in seconds
s	2.904012	1391.4
Cos α	9.943213	(458.9)
B	8.510900	1503
h	1.358125	1st term 22.8100
s²	5.808024	
Sin² α	9.36194	
C	1.31845	
	6.48841	2d term +.0003
h²	2.71624	
D	2.38338	
	5.09	3d term + ~
		−Δφ 22.810

	°	'	"	Values in seconds
½(φ+φ')	39	21	33.7	
	Logarithms			
s	2.904012			326.12
Sin α	9.680971			(1110.141
A'	8.509135			1436.26
Sec φ'	0.111739			
Δλ	1.205857			16.064
Sin ½(φ+φ')	9.802214			
−Δα	1.008071			10.18

11—9362 U. S. GOVERNMENT PRINTING OFFICE, 1929

DEPARTMENT OF COMMERCE
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POSITION COMPUTATION, THIRD-ORDER TRIANGULATION

			°	′	″
α	2 T.P.7	to 3 T.P.6	28	40	07.5
2d ∠		&	+57	06	19.2
α	2 T.P.7	to 1 T.P.8	79	46	26.7
Δα				−1	10.7
			180	00	00.0
α′	1 T.P.8	to 2 T.P.7	259	45	16.0

			°	′	″
α	3 T.P.8	to 2 T.P.7	259	45	16.0
3d ∠		&	−180	51	26.7
α	3 T.P.8	to 1 T.P.9	80	36	42.7
Δα				−	8.7
			180	00	00.0
α′	1 T.P.9	to 3 T.P.8	260	36	34.0

First Angle of Triangle

	°	′	″		λ	°	′	″
φ	39	21	45.118	2 T.P.7	λ	74	37	13.620
Δφ		−	15.624	2711.5	Δλ	−	1	51.458
φ′	39	21	29.494	1 T.P.8	λ′	74	39	05.078

	°	′	″		λ	°	′	″
φ	39	21	29.494	3 T.P.8	λ	74	39	05.078
Δφ		−	1.756	331.97	Δλ		+	13.680
φ′	39	21	27.738	1 T.P.9	λ′	74	39	18.758

	Logarithms	Values in seconds
s	3.433 216	909.6 + (940.8)
Cos α	9.249 272	
B	8.510 900	
h	1.193 388	1st term + 15.609
s²	6.856 61	
Sin²α	9.98609	
C	1.31855	
	8.161.25	2d term + .0145
h²	2.3769	
D	2.3838	
	~	3d term +
		−Δφ 15.624

	°	′	″	Logarithms	Values in seconds
½(φ+φ′)	39	21	37.4		
s				3.433 216	121.6 + (1314.9)
Sin α				9.993 046	
A′				8.509 135	
Sec φ′				0.111 710	
Δλ				2.047 107	+111.458
Sin ½(φ+φ′)				9.802 223	
−Δα				1.849 330	70.68

	Logarithms	Values in seconds
s	2.521 099	855.4 + (9949)
Cos α	9.212 512	
B	8.510 900	
h	0.244 511	1st term 1.754
s²	5.042 19	
Sin²α	9.99828	
C	1.31850	
	6.34897	2d term + .002
h²		
D	2.3838	
	~	3d term +
		−Δφ

	°	′	″	Logarithms	Values in seconds
½(φ+φ′)	39	21	28.8		
s				2.521 099	449.1 + (987.4)
Sin α				9.994 144	
A′				8.509 135	
Sec φ′				0.111 708	
Δλ				1.136 086	13.680
Sin ½(φ+φ′)				9.802 202	
−Δα				0.938 288	.8675

11—9362 U. S. GOVERNMENT PRINTING OFFICE: 1929

DEPARTMENT OF COMMERCE
U. S. COAST AND GEODETIC SURVEY
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POSITION COMPUTATION, THIRD-ORDER TRIANGULATION

			°	′	″
α	2 T.P. 9	to 3 T.P. 8	260	36	24.0
2d ∠		&	+200	55	48.3
α	2 T.P. 9	to 1 T.P. 10	101	32	22.3
Δα				−	17.8
			180	00	00.0
α′	1 T.P. 10	to 2 T.P. 9	281	32	04.5

			°	′	″
α	3 T.P. 10	to 2 T.P. 9	281	32	04.5
3d ∠		&	+171	43	29.2
α	3 T.P. 10	to 1 T.P. 11	93	15	33.7
Δα				−	12.8
			180	00	00.0
α′	1 T.P. 11	to 3 T.P. 10	273	15	20.9

First Angle of Triangle

	°	′	″			°	′	″
φ	39	21	27.738	2 T.P. 9	λ	74	39	18.758
Δφ		+	4.457	687.26	Δλ		+	28.126
φ′	39	21	32.195	1 T.P. 10	λ′	74	39	46.884

	°	′	″			°	′	″
φ	39	21	32.195	3 T.P. 10	λ	74	39	46.884
Δφ			+.895	485.82	Δλ		+	20.259
φ′	39	21	33.090	1 T.P. 11	λ′	74	40	07.143

	Logarithms	Values in seconds
s	2.837 121	−992.88 (857.49)
Cos α	9.301 126	
B	8.510 900	
h	0.649 147	1st term 4.457 81
s²	567424	
Sin² α	9.982 26	
C	1.318 50	
	6.975 00	2d term +.0009
h²	—	
D	2.3838	
	—	3d term + —
		−Δφ − 4.457

	°	′	″	Logarithms	Values in seconds
½(φ+φ′)	39	21	30.1		
s				2.837 121	
Sin α				9.991 131	+1122.45 (314.00)
A′				8.509 135	
Sec φ′				0.111 716	
Δλ				1.449 103	28.126
Sin ½(φ+φ′)				9.802 205	
−Δα				1.253 1308	−17.83

	Logarithms	Values in seconds
s	2.686 475	−1023.57 (829.89) ✓
Cos α	8.754 776	
B	8.510 900	
h	9.952 151	1st term −.895 74
s²	537295	
Sin² α	999859	
C	1.318 50	
	6.690 04	2d term +.0005
h²		
D	2.3838	
		3d term +
		−Δφ − .895

	°	′	″	Logarithms	Values in seconds
½(φ+φ′)	39	21	32.8		
s				2.686 475	
Sin α				9.999 297	+171.9 (1266.2)
A′				8.509 135	
Sec φ′				0.111 717	
Δλ				1.306 624	+20.2593
Sin ½(φ+φ′)				9.802 212	
−Δα				1.108 836	+12.84

11—9362 U. S. GOVERNMENT PRINTING OFFICE, 1929

1847

DEPARTMENT OF COMMERCE
U. S. COAST AND GEODETIC SURVEY
Form 27
Ed. April, 1929

POSITION COMPUTATION, THIRD-ORDER TRIANGULATION

			°	'	"
α	2 T.P.11	to 3 T.P.10	273	15	20.9
2d ∠		&	+206	10	10.0
α	2 T.P.11	to 1 T.P.12	119	25	30.9
Δα				−	6.6
			180	00	00.0
α′	1 T.P.12	to 2 T.P.11	299	25	24.3

			°	'	"
α	3 T.P.12	to 2 T.P.11	299	25	24.3
3d ∠		&	+161	00	37.5
α	3 T.P.12	to 1 End	100	26	01.8
Δα				−	6.3
			180	00	00.0
α′	1 End	to 3 T.P.12	280	25	55.5

First Angle of Triangle

		°	'	"			°	'	"
φ	39	21	33.090	2 T.P.11	λ	74	40	07.143	
Δφ		+	4.553	285.81	Δλ		+	10.398	
φ′	39	21	37.643	1 T.P.12	λ′	74	40	17.541	

		°	'	"			°	'	"
φ	39	21	37.643	3 T.P.12	λ	74	40	17.541	
Δφ		+	1.421	242.04	Δλ		+	9.943	
φ′	39	21	39.064	1 End	λ′	74	40	27.484	

	Logarithms	Values in seconds
s	4.456077	11 60.90
Cos α	9.691 338	(689.46)
B	8.510 900	
h	0.658 31[3]	1st term 45.532
s²	4.912 15	
Sin²α	9.88003	
C	1.31850	
	6.11068	2d term +.0001
h²		
D	2.38388	3d term +
		−Δφ 4.553

	° ' "
½(φ+φ′)	39-21-35.5

	Logarithms	Values in seconds
s	2.456077	419.94
Sin α	9.940 016	(1016.51)
A′	8.509 135	
Sec φ′	0.111 725	
Δλ	1.016 953	10.398
Sin ½(φ+φ′)	9.80 2219	
−Δα	0.819 172	6.594

	Logarithms	Values in seconds
s	4.383 887	1204.7
Cos α	9.257 918	(645.6)
B	8.510 900	
h	0.152 705	1st term 142.14
s²	4.76777	
Sin²α	9.98551	
C	1.31850	
	6.07178	2d term +.0001
h²		
D		3d term +
		−Δφ 1.421

	° ' "
½(φ+φ′)	39-21-34.0

	Logarithms	Values in seconds
s	2.383 887	
Sin α	9.992 758	+ 658.0
A′	8.509 135	(778.5)
Sec φ′	0.111 719	
Δλ	0.997 499	9.9426
Sin ½(φ+φ′)	9.80 2216	
−Δα	0.799 715	6.305

11—9352 U. S. GOVERNMENT PRINTING OFFICE: 1929

DEPARTMENT OF COMMERCE
U. S. COAST AND GEODETIC SURVEY
Form 27
Ed. April, 1929

POSITION COMPUTATION, THIRD-ORDER TRIANGULATION

			°	′	″
α	2 Apple	to 3 A2 Mark	224	56	43.7
2d ∠	Apple	& A2 Mark	+326	04	01
α	2 Apple	to 1 T.P.1	191	00	44.7
Δα			551	+	1.7
			180	00	00.0
α′	1 T.P.1	to 2 Apple	11	00	464

			°	′	″
α	3 T.P.1	to 2 Apple	11	00	46.4
3d ∠		&	+213	14	57.5
α	3 T.P.1	to 1 T.P.2	224	15	43.9
Δα				+	15.3
			180	00	00.0
α′	1 T.P.2	to 3 T.P.1	44	15	59.2

First Angle of Triangle

	°	′	″			°	′	″
φ	39	20	55.529	2 Apple	λ	74	42	03.267
Δφ		+	10.526	330.70	Δλ		−	2.638
φ′	39	21	06.055	1 T.P.1	λ′	74	42	00.629

	°	′	″			°	′	″
φ	39	21	06.055	3 T.P.1	λ	74	42	00.629
Δφ		+	19.216	829.423	Δλ	−		24.179
φ′	39	21	25.271	1 T.P.2	λ′	74	41	36.450

	Logarithms	Values in seconds
s	2.5194342	186.7 (1683.6)
Cos α	9.9919282	
B	8.5109011	
h	1.0222635	1st term 10.5260
s²	5.03887	
Sin² α	8.5616	
C	1.31835	
	4.91938	2d term +
h²	2.04	
D	2.3838	
		3d term +
		−Δφ −10.5266

	°	′	″	Logarithms	Values in seconds
½(φ+φ′)	39	21	00.79		
s				2.5194342	−15.06
Sin α				9.2810828	1421.6
A′				8.509 1349	
Sec φ′				0.111 6696	
Δλ				0.42132 15	−2.6382
Sin ½(φ+φ′)				9.802 43296	
−Δα				0.22 37591	−1.674
				0.2234511	

	Logarithms	Values in seconds
s	2.9187760	780.70 (1069.67)
Cos α	9.8540061	−192609
B	8.5109011	
h	1.2836832	1st term 19.2169
s²	5.837655	
Sin² α	9.68764	
C	1.31836	
	6.84355	2d term + .0007
h²	2.5673	
D	2.3838	
	4.9511	3d term +
		−Δφ 19.216
		−19.2603

	°	′	″	Logarithms	Values in seconds
½(φ+φ′)	39	21	15.66		
s				2.9187760	872.71
Sin α				9.8438199	−(563.87)
A′				8.509 1348	
Sec φ′				0.111 7029	
Δλ				1.3834336	24.1787
Sin ½(φ+φ′)				9.8021678	
−Δα				1.1856014	15.3227

11—9362 U. S. GOVERNMENT PRINTING OFFICE, 1929

DEPARTMENT OF COMMERCE
U. S. COAST AND GEODETIC SURVEY
FORM 27
Ed. April, 1929

POSITION COMPUTATION, THIRD-ORDER TRIANGULATION

			°	′	″
α	2 T.P.2	to 3 T.P.1	44	15	59.2
2d ∠		&	+184	53	01.5
α	2 T.P.2	to 1 T.P.3	229	09	00.7
Δα				+	7.1
			180	00	00.0
α′	1 T.P.3	to 2 T.P.2	49	09	07.8

			°	′	″
α	3 T.P.3	to 2 T.P.2	49	09	07.8
3d ∠		&	+89	23	47.1
α	3 T.P.3	to 1 T.P.4	138	32	54.9
Δα				−	5.3
			180	00	00.0
α′	1 T.P.4	to 3 T.P.3	318	32	49.6

FIRST ANGLE OF TRIANGLE

	°	′	″		λ	°	′	″
φ	39	21	25.315	2 T.P.2	λ	74	41	36.450
Δφ		+	7.560	356.452	Δλ		−	11.262
φ′	39	21	32.875	1 T.P.3	λ′	74	41	25.188

	°	′	″		λ	°	′	″
φ	39	21	32.875	3 T.P.3	λ	74	41	25.188
Δφ		+	7.397	304.3586	Δλ		+	8.416
φ′	39	21	40.272	1 T.P.4	λ′	74	41	33.604

	Logarithms	Values in seconds
s	2.5520010	1013.85
Cos α	9.8156298	(836.52)
B	8.5109005	
h	0.8785313	1st term 7.56017
s²	5.10400	
Sin²α	9.75753	
C	1.31847	
	6.18000	2d term +.00015
h²	1.757	
D	2.3838	
	4.0	3d term + —
	−	−Δφ 7.560

	°	′	″	Logarithms	Values in seconds
½(φ+φ′)	39	21	29.09		
s				2.5520010	602.98
Sin α				9.8787669	(833.51)
A′				8.5091346	
Sec φ′				0.1117160	
Δλ				1.0516185	11.262
Sin½(φ+φ′)				9.8022022	
−Δα				0.8538207	7.1420

	Logarithms	Values in seconds
s	2.4833855	1241.98
Cos α	9.8747817	(608.40)
B	8.5109004	
h	0.8690676	1st term 7.3972
s²	4.9666771	
Sin²α	9.64169	
C	1.31850	
	4.9626961	2d term +.0008
h²	1.9335	
D	2.3838	
		3d term + —
		−Δφ 7.397

	°	′	″	Logarithms	Values in seconds
½(φ+φ′)	39	21	36.57		
s				2.4833855	804.47
Sin α				9.8208479	(631.90)
A′				8.5091346	
Sec φ′				0.1117287	
Δλ				0.9250967	84.158
Sin½(φ+φ′)				9.8022213	
−Δα				0.7273180	5.337

11—9362 U. S. GOVERNMENT PRINTING OFFICE, 1930

DEPARTMENT OF COMMERCE
U. S. COAST AND GEODETIC SURVEY
Form 27
Ed. April, 1929

POSITION COMPUTATION, THIRD-ORDER TRIANGULATION

			°	′	″
α	2 T.P.4 to 3 T.P.3		318	32	49.6
2d ∠	&		+312	49	32.1
α	2 T.P.4 to 1 End.		271	22	21.7
Δα			631	+	42.0
			180	00	00.0
α′	1 End. to 2 T.P.4		91	23	03.7

			°	′	″
α	3 to 2				
3d ∠	&		−		
α	3 to 1				
Δα					
			180	00	00.0
α′	1 to 3				

First Angle of Triangle

	°	′	″			°	′	″
φ	39	21	40.272	2 T.P.4	λ	74	41	33.604
Δφ		−	1.236	1584.56	Δλ		−1	06.168
φ′	39	21	39.036	1 End.	λ′	74	40	27.436

	°	′	″			°	′	″
φ				3	λ			
Δφ					Δλ			
φ′				1	λ′			

	Logarithms	Values in seconds
s	3.199 9087	1203.86
Cos α	8.379 4097	+ (646.51)
B	8.510 9002	
h	0.0902 186	1st term 123″089
s²	6.399 91	
Sin² α	9.999 75	
C	1.31 854	
	7.718 20	2d term +.0052
h²	0.1804	
D	2.3839	
		3d term +
	+	−Δφ 1.236

	°	′	″	Logarithms	Values in seconds
½(φ+φ′)	39	21	39.65		
s				3.199 9087	656.79
Sin α				9.999 3753	− (779.51)
A′				8.509 1346	
Sec φ′				0.111 7265	
Δλ				1.820 6451	−66″1676
Sin ½(φ+φ′)				9.802 2294	
−Δα				1.622 8745	41.963

	Logarithms	Values in seconds
s		
Cos α		
B		
h		1st term ″
s²		
Sin² α		
C		
		2d term +
h²		
D		
		3d term +
		−Δφ

	°	′	″	Logarithms	Values in seconds
½(φ+φ′)					
s					
Sin α					
A′					
Sec φ′					
Δλ					″
Sin ½(φ+φ′)					
−Δα					

11—9362 U. S. GOVERNMENT PRINTING OFFICE, 1929

44 40

	Remarks	Decisions
1		
2		
3		
4		Omit s
5		
6		
7		Omit s
8	* 'landing' (initial letter, lower case) because landing is not a part of Geog. Name, it being a landing for village English Creek	
9		
10		Approved by U.S.G.B. Sixth Report.
11		
12		
13		
14		Not Jeffries
15		
16		
17		
18		
19		
20		
21		
22		
23		
24		
25		
26		
27		

M 234

GEOGRAPHIC NAMES

Survey No. T-5641

Name on Survey	A: On Chart No. 1217	B: On previous survey No. T-1468 & T-2054	C: On U. S. quadrangle Maps	D: From local information (in Arrears) Soil Map N.J. State of N.J. Dept. of Agriculture Millville sheet	E: On local Maps Cons & Devel No. 36	F: P. O. Guide or Map	G: Rand McNally Atlas	H: U. S. Light List	K: U.S.G.B. Sixth Report	
Oakville			✓	✓	✓					1
Gibson Landing			✓	Gibson's Ldg.	Gibson's Ldg.					2
Gibson Creek			Gibson's Cr.	✓	Gibson's ~~Ldg~~ Cr.					3
Scull's Landing			Scull Ldg.	✓	✓					4
Powell Creek			Powell's Cr.	✓	Powell's Creek					5
English Creek			✓	✓	✓					6
Nell's Run			Nell Run	✓	✓					7
English Creek ~~Landing~~ landing	*		✓	✓	✓					8
Scullville			Jeffers	✓	✓	✓	✓			9
Great Egg River	✓	Great Egg Harbour River	Great Egg Harbor R.	✓	Great Egg Harbor R.	✓	Great Egg Harbor R.		✓	10
Lakes Creek			Lake's Cr.	✓	✓					11
Sedge Creek			✓		✓					12
Middle River	✓	✓	✓	-	✓					13
~~Jeffries~~ Jeffers Landing	✓	✓	✓	Jeffers Ldg.	Jeffers Ldg.					14
Job Point	✓	Job's Point	✓	Jobs Pt.	Job's Point					15
										16
English Creek (the settlement)			✓		✓		✓			17
										18
										19
										20
										21
										22
										23
										24
										25
										26
										27

Names underlined in red approved by GFE on 12/14/36

M 234

M-350

T-5641

PLANE COORDINATE GRID SYSTEM

Positions of grid intersections used for fitting the grid to this compilation were computed by Division of Geodesy and the computation forms are included in this report.

Positions plotted by R. E. Ask

Positions checked by R. E. Ask

Grid inked on machine by R. E. Ask

Intersections inked by W. H. Schleeter

Points used for plotting grid:

x 1,990,000 ft y 180,000	x 1,980,000 y 190,000
x 2,005,000 y 175,000	x y
x 2,005,000 y 190,000	x y
x 1,980,000 y 175,000	x y

Triangulation stations used for checking grid:

X = 2,004,285.64' y = 176,331.67'

1. Jeff 1935 (ref. sta.)
2. Apple 1935
3. Electric, W. 1935
4. Gibson 1935
5.
6.
7.
8.

Form No. 743
DEPARTMENT OF COMMERCE
U. S. COAST AND GEODETIC SURVEY
Ed. May 1935

T-5641a

GEODETIC POSITIONS FROM TRANSVERSE MERCATOR COORDINATES

STATE N. J. STATION

x	1,990,000.00	$\log S_g$	4. 0000000000
K	2,000,000.00	$\log (1200/3937)$	9.4840158 3
x' $(=x-K)$	− 10,000.00	$\log (1/R)$	0086
$x'^3/(6\rho_o^2)_g$	+ .00	$\log S_m$	3.4840 2669
S_g	− 10,000.00	cor. arc to sine	− 2
		$\log S_1$	3.4840 2667
3 log x'	2.0000000000	$\log A$	8.5041 3543
$\log 1/(6\rho_o^2)_g$	4.5810231	$\log \sec \phi$	0.1115 4468
$\log x'^3/(6\rho_o^2)_g$	6.5810231	$\log \Delta\lambda_1$	2.1046 4178
		cor. sine to arc	+ 3
$\log S_m^2$	6.9680 5338	$\log \Delta\lambda$	2.1046 8181
$\log C$	1.3148021	$\Delta\lambda$	127.2570
$\log \Delta\phi$	4.2460 74		
y	180,000.00		
ϕ' (by interpolation)	39° 19' 39.1831	λ (central mer.)	74° 40' 00.0000
$\Delta\phi$	− .0193	$\Delta\lambda$	+ 2 07.2570
ϕ	39 19 39.1638	λ	74 42 07.2570
	120.77 mm		17.39 mm

Explanation of form:

$x'=x-K$

$S_g=x'-\frac{x'^3}{(6\rho_o^2)_g}$

$S_m=\frac{1}{R}\left(\frac{1200}{3937}\right)S_g$

R=scale reduction factor

ϕ' is interpolated from table of y

$\Delta\phi=C\,S_m^2$

$\phi=\phi'-\Delta\phi$

$\Delta\lambda_1=S_1 A \sec\phi$

$\log S_1=\log S_m-$cor. arc to sine

$\log \Delta\lambda=\log \Delta\lambda_1+$cor. arc to sine

$\lambda=\lambda$ (central mer.)$-\Delta\lambda$

U. S. GOVERNMENT PRINTING OFFICE 11—11521

T-5641 b

Form No. 743
DEPARTMENT OF COMMERCE
U. S. COAST AND GEODETIC SURVEY
Ed. May 1935

GEODETIC POSITIONS FROM TRANSVERSE MERCATOR COORDINATES

STATE N. J. STATION

x	2,005,000.00	$\log S_g$	3.69897000
K	2,000,000.00	$\log (1200/3937)$	9.48401583
x' $(=x-K)$	+ 5,000.00	$\log (1/R)$	1086
$x'^3/(6\rho_o^2)_g$	— .00	$\log S_m$	3.18299669
S_g	+ 5,000.00	cor. arc to sine	— 0
		$\log S_1$	3.18299669
$3 \log x'$	1.09691000	$\log A$	9.50913577
$\log 1/(6\rho_o^2)_g$	4.58102311	$\log \sec \phi$	0.11143448
$\log x'^3/(6\rho_o^2)_g$	5.67793311	$\log \Delta\lambda_1$	1.80356694
		cor. sine to arc	+ 0
$\log S_m^2$	6.36599338	$\log \Delta\lambda$	1.80356694
$\log C$	1.31748 10	$\Delta\lambda$	63.61611
$\log \Delta\phi$	7.68380 3		
y	175,000.00		
ϕ' (by interpolation)	39° 18' 49.7634	λ (central mer.)	74° 40' 00.0000
$\Delta\phi$	— .0048	$\Delta\lambda$	— 1 03.6161
ϕ	39 18 49.7586	λ	74 38 56.3839
	153.45 mm		135.11 mm

Explanation of form:

$x' = x - K$

$S_g = x' - \frac{x'^3}{(6\rho_o^2)_g}$

$S_m = \frac{1}{R}\left(\frac{1200}{3937}\right) S_g$

R=scale reduction factor

ϕ' is interpolated from table of y

$\Delta\phi = C\, S_m^2$

$\phi = \phi' - \Delta\phi$

$\Delta\lambda_1 = S_1 A \sec \phi$

$\log S_1 = \log S_m - \text{cor. arc to sine}$

$\log \Delta\lambda = \log \Delta\lambda_1 + \text{cor. arc to sine}$

$\lambda = \lambda \text{ (central mer.)} - \Delta\lambda$

U. S. GOVERNMENT PRINTING OFFICE 11—11521

Form No. 743
DEPARTMENT OF COMMERCE
U. S. COAST AND GEODETIC SURVEY
Ed. May 1935

T-5641c

GEODETIC POSITIONS FROM TRANSVERSE MERCATOR COORDINATES

STATE N. J. STATION

x	2,005,000.00	$\log S_g$	3.69857000
K	2,000,000.00	$\log (1200/3937)$	9.48401583
x' $(=x-K)$	+ 5,000.00	$\log (1/R)$	1086
$x'^3/(6\rho_o^2)_g$	− .00	$\log S_m$	3.18299669
S_g	+ 5,000.00	cor. arc to sine	− 0
		$\log S_1$	3.18299669
3 log x'	1.09691000	$\log A$	8.50913473
$\log 1/(6\rho_o^2)_g$	4.58102311	$\log \sec \phi$	0.11169029
$\log x'^3/(6\rho_o^2)_g$	5.67793311	$\log \Delta\lambda_1$	1.80342171
		cor. sine to arc	+ 1
$\log S_m^2$	6.36599336	$\log \Delta\lambda$	1.80382172
$\log C$	1.318443	$\Delta\lambda$	63.6534
$\log \Delta\phi$	7.684436		
y	190,000.00		
ϕ' (by interpolation)	39° 21′ 18.0221	λ (central mer.)	74° 40′ 00.0000
$\Delta\phi$	− .0048	$\Delta\lambda$	− 1′ 03.6534
ϕ	39° 21′ 18.0173	λ	74° 38′ 56.3466
	55.56 mm		134.92 mm

Explanation of form:

$x'=x-K$

$S_g=x'-\frac{x'^3}{(6\rho_o^2)_g}$

$S_m=\frac{1}{R}\left(\frac{1200}{3937}\right)S_g$

R=scale reduction factor

ϕ' is interpolated from table of y

$\Delta\phi=C\,S_m^2$

$\phi=\phi'-\Delta\phi$

$\Delta\lambda_1=S_1 A \sec\phi$

$\log S_1=\log S_m-$cor. arc to sine

$\log \Delta\lambda=\log \Delta\lambda_1+$cor. arc to sine

$\lambda=\lambda$ (central mer.)$-\Delta\lambda$

U. S. GOVERNMENT PRINTING OFFICE 11—11531

T-5641 d

Form No. 743
DEPARTMENT OF COMMERCE
U. S. Coast and Geodetic Survey
Ed. May 1935

GEODETIC POSITIONS FROM TRANSVERSE MERCATOR COORDINATES

STATE N. J. STATION

x	1,940,000.00	$\log S_g$	4.30103003
K	2,000,000.00	$\log (1200/3937)$	9.48401583
x' $(=x-K)$	−20,000.00	$\log (1/R)$	1086
$x'^3/(6\rho_o^2)_g$	−.00	$\log S_m$	3.78505672
S_g	−20,000.00	cor. arc to sine	−7
		$\log S_1$	3.78505665
3 log x'	2,9030 9000	$\log A$	8.50913577
$\log 1/(6\rho_o^2)_g$	4.5810 231	$\log \sec \phi$	0.11143436
$\log x'^3/(6\rho_o^2)_g$	7.4841131	$\log \Delta\lambda_1$	2.40562678
		cor. sine to arc	+11
$\log S_m^2$	7.5701 13544	$\log \Delta\lambda$	2.40562689
$\log C$	1.317810	$\Delta\lambda$	254.4643
$\log \Delta\phi$	4.4879 23		
y	175,000.00		
ϕ' (by interpolation)	39 18 49.7634	λ (central mer.)	74 40 00.0000
$\Delta\phi$	−.0773	$\Delta\lambda$	+ 4 14.4643
ϕ	39 18 49.6861	λ	74 44 14.4643
	153.22 mm		34.66 mm

Explanation of form:

$x'=x-K$

$S_g=x'-\frac{x'^3}{(6\rho_o^2)_g}$

$S_m=\frac{1}{R}\left(\frac{1200}{3937}\right)S_g$

R=scale reduction factor

ϕ' is interpolated from table of y

$\Delta\phi=C\,S_m^2$

$\phi=\phi'-\Delta\phi$

$\Delta\lambda_1=S_1 A \sec\phi$

$\log S_1=\log S_m-$cor. arc to sine

$\log \Delta\lambda=\log \Delta\lambda_1+$cor. arc to sine

$\lambda=\lambda$ (central mer.)$-\Delta\lambda$

U. S. GOVERNMENT PRINTING OFFICE 11—11521

Form No. 743
DEPARTMENT OF COMMERCE
U. S. COAST AND GEODETIC SURVEY
Ed. May 1935

T-5641e

GEODETIC POSITIONS FROM TRANSVERSE MERCATOR COORDINATES

STATE N. J. STATION

x	1,980,000.00	$\log S_g$	4.30103003
K	2,000,000.00	$\log (1200/3937)$	9.48401583
x' $(=x-K)$	−20,000.00	$\log (1/R)$	.1086
$x'^3/(6\rho_o^2)_g$	.00	$\log S_m$	3.78505672
S_g	−20,000.00	cor. arc to sine	− 7
		$\log S_1$	3.78505665
$3 \log x'$	2.90309000	$\log A$	8.50973473
$\log 1/(6\rho_o^2)_g$	4.58102137	$\log \sec \phi$	0.11164016
$\log x'^3/(6\rho_o^2)_g$	7.48411137	$\log \Delta\lambda_1$	2.40548154
		cor. sine to arc	+ 11
$\log S_m^2$	7.57011344	$\log \Delta\lambda$	2.40548165
$\log C$	1.3184443	$\Delta\lambda$	254.6136
$\log \Delta\phi$	4.8848556		
y	190,000.00		
ϕ' (by interpolation)	39° 21′ 18.0221″	λ (central mer.)	74° 40′ 00.0000″
$\Delta\phi$	− .0774	$\Delta\lambda$	+ 4 14.6136
ϕ	39 21 17.9447	λ	74 44 14.6136
	55.34 mm		34.99 mm

Explanation of form:

$x' = x - K$

$S_g = x' - \frac{x'^3}{(6\rho_o^2)_g}$

$S_m = \frac{1}{R}\left(\frac{1200}{3937}\right) S_g$

R=scale reduction factor

ϕ' is interpolated from table of y

$\Delta\phi = C\, S_m^2$

$\phi = \phi' - \Delta\phi$

$\Delta\lambda_1 = S_1 A \sec \phi$

$\log S_1 = \log S_m$ − cor. arc to sine

$\log \Delta\lambda = \log \Delta\lambda_1$ + cor. arc to sine

$\lambda = \lambda$ (central mer.) $- \Delta\lambda$

U. S. GOVERNMENT PRINTING OFFICE 11—11621

REVIEW OF AIR PHOTO COMPILATION NO.

Chief of Party: E. H. Kirsch Compiled by: W. W. King

Project: H. T. 205 Instructions dated: May 16th, 1935

1. The charts of this area have been examined and topographic information necessary to bring the charts up to date is shown on this compilation. (Par. 16a, b,c,d,e,g and i; 26; and 64)

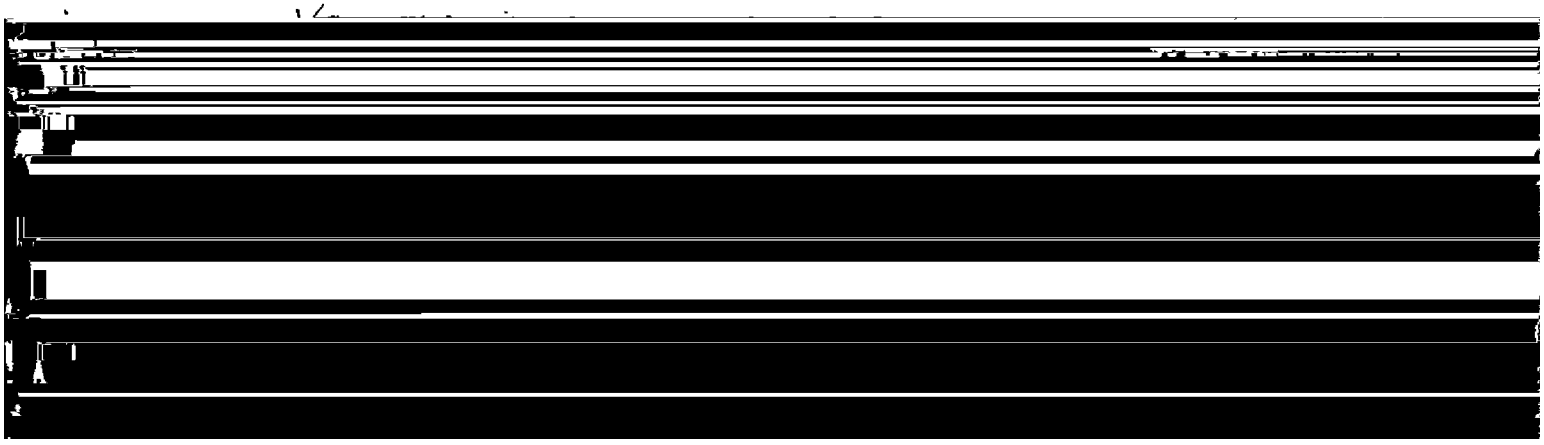
2. Change in position, or non-existence of wharfs, lights, and other topographic detail of particular importance to navigation which affect the chart, is discussed in the descriptive report. (Par. 26; and 66 g,n)

3. Ground surveys by plane table, sextant, or theodolite have been used to supplement the photographic plot where necessary to obtain complete information, and all such surveys are discussed in the descriptive report. (Par. 65; and 66 d,e)

4. Blue-prints and maps from other sources which were transmitted by the field party contain sufficient control for their application to the charts. (Par. 28)

5. Differences between this compilation and contemporary plane table and hydrographic surveys have been examined and rectified in the field before forwarding the compilations to the office and are discussed in the descriptive report.

6. The control and adjustment of the photo plot are discussed in the descriptive report. Unusual or large adjustments are discussed in detail and limits of the area affected are stated. (Par. 12b; 44; and 66 c,h,i)



✓8. The representation of low water lines, reefs, coral reefs and rocks and legends pertaining to them is satisfactory. (Par.

[redacted]

✓9. Recoverable objects have been located and described on Form 524 in accordance with circular 30, 1933, circular letter of March 3, 1933, and circular 31, 1934. (Par. 29, 30, and 57)

✓10. A list of landmarks was furnished on Form 567 and instructions in the Director's letter of July 16, 1934, Landmarks for Charts, complied with. (Par. 16d, e; and 60)

✓11. All bridges shown on the compilation are accompanied by a note stating whether fixed or draw, clearance, and width of draw if a draw bridge. Additional information of importance to navigation is given in the descriptive report. (Par. 16c)

Overhead Cable Crossing. Crosses Great Egg River near lat. 39° 19' 40", long 74° 40' 50". The two supporting towers are about 150 feet high with a cable clearance of about 100 feet.

✓12. Geographic names are shown on the overlay tracing. The accepted local usage of new names has been determined and they are listed in the report, together with a general statement as to source of information and a specific statement when advisable. Complete discussion of place names differing from the charts and from the U. S. G. S. Quadrangles is given in the descriptive report, together with reasons for recommendations made. (Par. 64, and 66k)

✓13. The geographic datum of the compilation is N. A. 1927 and the

T-2054 (1891) 1:20,000, which covers the southeastern portion of T-5641 is the only previous survey in this area. The general agreement of shoreline is good, however there have been several changes in detail. T-5641 is adequate to supersede T-2054 over the common area.

3. All station points are exactly marked by fine black dots.

4. Closely spaced lines are drawn sharp and clear for printing.

5. Topographic symbols for similar features are of uniform weight.

6. All drawing has been retouched where partially rubbed off.

7. Buildings are drawn with clear straight lines and square corners where such is the case on the ground.

(Par. 34, 35, 36, 37, 38, 39, 40, 41, 42, 43, 44, 45, 46, 48)

16. No additional surveying is recommended at this time.

17. Remarks: ~~None~~ High water line is of the date of the photographs, April 22, 1932 as the field inspection showed no appreciable change.

18. Examined and approved;

E. H. Kraeh.
Chief of Party

19. Remarks after review in office: Hydrographic & Topographic surveys are contemplated for this area in 1937. Corrections and additions to T-5641 as a result of these surveys will be made when this work is completed.

Reviewed in office by: R. E. Ask
Frank G. Endicott

Examained and approved:

E. F. Green.
Chief, Section of Field Records

Fred. L. Peacock
Chief, Section of Field Work

L. O. Colbert
Chief, Division of Charts

G. Rude
Chief, Division of Hydrography and Topography.

Report for T 5641 Supplemental.

Corrections in red applied 5/24/38 by Whitman checked by E.W. Frederick.

a. Plane table survey of July 1937 (Field No WD) Office No. CS 119 M. All details within the area of T 5641 Supplemental applied to the supplemental

[redacted]