# HTDP 3.0: Software for Coping with the Coordinate Changes Associated with Crustal Motion

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**Abstract:** NOAA's National Geodetic Survey has developed the horizontal time-dependent positioning (HTDP) software to provide a way for its users to estimate the coordinate changes associated with horizontal crustal motion in the United States. HTDP contains a model for estimating horizontal crustal velocities and separate models for estimating the displacements associated with 29 earthquakes (two in Alaska and 27 in California). This software is updated periodically to provide more accurate estimates for crustal velocities and earthquake displacements, as well as to include models for additional earthquakes. In June 2008, NGS released version 3.0 of HTDP (HTDP 3.0) that introduces an improved capability for predicting crustal velocities, based on a tectonic block model of the western contiguous United States (CONUS), that is, from the Rockies to the Pacific coast. Values for the model parameters that predict the velocity at any point within the domain were estimated from 4,890 horizontal velocity vectors (derived from repeated geodetic observations), 170 fault slip rates, and 258 fault slip vector azimuths. Extensive testing indicates that this model can predict velocities within CONUS with a standard error of less than 2 mm/year in both the north and east components. HTDP 3.0 also introduces a model for the combined coseismic and postseismic displacements associated with the magnitude 7.9 Denali earthquake that occurred in central Alaska on November 3, 2002.

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#### Introduction

In 1992, NOAA's National Geodetic Survey (NGS) introduced the first version of the horizontal time-dependent positioning (HTDP) software for providing the geospatial community a way to estimate changes in horizontal positional coordinates associated with crustal motion [www.ngs.noaa.gov/TOOLS/Htdp/Htdp.shtml; see also Snay (1999, 2003)]. In particular, the HTDP software contains models for horizontal crustal velocities in the United States. This software also contains models that predict the horizontal displacements associated with several major U.S. earthquakes. NGS has since released new versions of HTDP with revised models on several occasions to improve the accuracy of the estimated velocities and to include models for additional earthquakes.

In June 2008, NGS released version 3.0 of HTDP (HTDP 3.0)

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which incorporates the newest model for predicting horizontal crustal velocities in the western part of the contiguous United States (CONUS). HTDP 3.0 also introduces a model for predicting the displacements associated with the magnitude 7.9 Denali earthquake, which devastated central Alaska on November 3, 2002. This paper describes these new models, plus it addresses other recent revisions to the HTDP software.

Estimating the horizontal surface velocity for a user-specified location is one of two primary functions supported by HTDP. The software's second primary function is to predict horizontal displacements for a user-specified location and a user-specified period of time. For this second function, HTDP multiplies the predicted velocity by the time difference and then adds any earthquake-related displacements that occurred during the specified time period. In predicting velocities and/or displacements, HTDP applies numerical models for horizontal crustal motion which have been derived from repeated geodetic observations, as well as from geological, seismological, and other geophysical information.

The reality of crustal motion implies that positional coordinates in many locations change as a function of time. Hence, it is inappropriate to specify positional coordinates for these locations without also specifying the date to which these coordinates correspond. Let us call this date the *reference date* for the given coordinates. People may apply HTDP to update (or backdate) the positional coordinates of a point from one reference date to corresponding coordinates for another reference date. This software simply adds (or subtracts) the point's predicted displacement between the two dates to the positional coordinates of the starting reference date.

HTDP also enables its users to update (or backdate) certain types of geodetic observations [differential global positioning sys-

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tem (GPS), distances, azimuths, horizontal angles, horizontal directions] from the value that was measured on the day of observation to the value that would have been measured on some other date. Indeed, as part of the NSRS2007 readjustment of NAD 83, NGS updated all pertinent GPS observations that were observed in California between 1986 and 2005 to corresponding values that would have been observed on January 1, 2007. NGS then performed a simultaneous (fixed-Earth) adjustment of these updated observations to determine the NAD 83 (NSRS2007) positional coordinates for over 1,000 reference stations that provide geodetic control for California (Pearson 2005). The need to update observations to a common date, called data homogenization, is a burden of living in earthquake country; but this need is not unique to California.

HTDP 3.0 predicts velocities primarily relative to the International Terrestrial Reference Frame of 2005 (ITRF2005) (Altamimi et al. 2007), but it is able to convert these predicted values to equivalent values in other popular reference frames, including all other realizations of ITRF, all realizations of the World Geodetic System of 1984 (WGS84), and to the CORS96 realization of the North American Datum of 1983 [NAD 83 (CORS96)]. Consequently, HTDP 3.0 may be used to transform positional coordinates and/or velocities from one reference frame to another in a manner that rigorously accounts for the relative motion between these frames. The NGS-adopted transformation equations between ITRF2005 and NAD 83 (CORS96) are given in the Appendix of this paper.

#### **Nature of Crustal Motion**

Since the 1960s geologists have known that the Earth's surface is partitioned into a number of tectonic plates that are in constant motion relative to each other at rates which are typically about several centimeters per year. These plates generally move as rigid blocks; however, at their edges there is a zone (often called a plate boundary) where they rub against each other and deform, causing earthquakes and other geophysical phenomena. CONUS straddles the boundary between the North American plate and the Pacific plate within the part of California located south of Mendocino, California. In the northwest corner of CONUS, the North American plate is colliding with the oceanic Juan de Fuca plate and its smaller neighbors: the Gorda and Explorer plates. Moreover, the Pacific coast of Alaska resides in the deformation zone associated with the boundary between the North American plate and the Pacific plate. As a result, most of California, Nevada, Oregon, Washington and Alaska are undergoing crustal deformation. Like other continental plate boundaries, the deformation extends hundreds of kilometers to either side of the boundary proper. As such, the deformation in CONUS extends eastward, though at a lower rate, as far as Salt Lake City, Yellowstone, and the Rio Grande Rift.

In the ITRF and WGS84 reference frames, all points on both the Pacific and North American plates have nonzero velocities reflecting the movement of the plates (Snay and Soler 2000). The NAD 83 reference frame, however, is defined so that all points on the North American plate, located sufficiently far from the plate boundary zone, will have (on average) zero horizontal velocities. Points located within the Pacific-North American plate boundary zone will have NAD 83 velocities that are transitional between the respective velocities of these two plates and as a result have nonzero NAD 83 velocities with magnitudes of up to 5 cm/yr, the Pacific plate velocity.

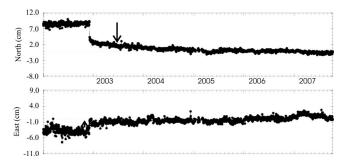
The deformation modeled by HTDP is largely caused by the tectonic plates that interact within the western margin of North America. Much of the motion is assumed to be accommodated by geologic faults that extend from Earth's surface to points deep within Earth's crust. The crust, however, is comprised of two layers that deform in quite different ways. These layers are separated by a broad zone called the brittle-ductile transition zone. In the top layer (known as the brittle region) rocks deform following the same elastic principles as ordinary engineering materials. Here, deformation causes increasing stress that eventually exceeds the frictional strength of the faults leading to an earthquake. Deeper in the crust, where conditions are hotter, the rocks behave in a ductile manner. Here deformation occurs by a slow continuous process and stress never reaches a value sufficient to cause catastrophic failure.

As a result, two quite different processes are responsible for the deformation in the western states. The first of these is slow response of the deeper part of the crust and the elastic response of the upper crust to the differential movement of the tectonic plates. It is assumed that faults in the lower crust accommodate this motion by slipping without earthquakes and this deformation is transmitted through the elastic crust to the surface and causes the secular velocity field. While the resulting secular velocities are fairly small, up to about 5 cm/year in some places, the effect on the positions of surface points accumulates with time and is large enough that it cannot be ignored. The secular velocities are assumed to be relatively constant, so that once this part of the field is mapped, it need not be changed, although periodic updates are needed to reflect our improved knowledge of it. The second part is the displacement caused by earthquakes that result when elastic stress associated with the secular velocity field accumulates along a fault. At some instant, the force caused by the stress acting on the fault exceeds the frictional force which keeps the fault locked. In this case, a fault will suddenly slip and quite large displacements can happen within a period of a few minutes or less. This so-called coseismic portion of the deformation field is therefore different because earthquakes happen in unpredictable ways. So each time there is a new earthquake, the HTDP software must be updated with the appropriate parameters for modeling the deformation. Because these two processes are very different both temporally and spatially, two quite different methodologies are required to model them. The secular velocity field is represented by a two-dimensional grid-interpolation scheme of the velocity field that provides an estimate of the velocity of any point located within the plate boundary zone, while earthquakes are represented using dislocation models (Okada 1985; Savage 1980) that define the slip on related geologic faults.

# **Earthquakes**

The deformation associated with an earthquake is caused by a fault in the Earth that slips suddenly due to the stress in the surrounding rocks. Sometimes the break extends to the surface in which case the displacement will change very suddenly as one side of the fault will move one way while the opposite side moves in the opposite direction. Often, however, the break does not reach the surface. Even in this case, the earthquake will cause surface displacements because slip on the fault will cause sympathetic movement in the surrounding rocks and this deformation will propagate through the Earth to the surface. Slip on the fault, with its accompanying decrease in stress on the fault, allows the elastic material surrounding the fault to rebound as the elastic

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**Fig. 1.** Time series of coordinates for the CORS site, FAIR, for the period spanning the Denali earthquake. The time axis starts on December 2, 2001, or the first day when ITRF00 became operational. Major division correspond to 1 year of data while the minor ticks represent 30 days. The Denali earthquake occurred near the end of the first year of the time interval. The plots show both a sudden coseismic displacement and a more gradual exponential decay associated with postseismic slip. Arrows show the coseismic displacement associated with the Denali Earthquake as estimated with HTDP 3.0. These arrows can be compared with the step change in the north and east time series at the time of the earthquake.

strain in the surrounding rocks (caused by deformation associated with the secular velocity field) is released. This release in the elastic strain in the rocks surrounding the earthquake rupture results in deformation associated with the earthquakes extending a considerable distance from the fault. In large earthquakes, measurable coseismic displacement can extend hundreds of kilometers from the fault.

In small, shallow earthquakes, where the material near the fault is cool enough to be fully elastic, the deformation associated with the earthquake will be complete within a few minutes and coseismic deformation is all that will occur. However in larger or deeper earthquakes, the rupture may extend deep enough so that the bottom of the active part of the fault is near the brittle-ductile transition. The adjacent ductile parts of the crust will respond to the stress change caused by the earthquake in a viscous manner and the resulting deformation may last for several months or years. This slow deformation does not cause noticeable seismic waves or shaking and is called postseismic deformation (Freed 2005, 2007). Postseismic slip is important to surveyors because it contributes to the total deformation field on the surface that will affect the relative position of points causing them to change from the relationships measured during earlier surveys. HTDP currently includes no mechanism for realistically modeling postseismic motion because the effect is usually small compared to coseismic deformation and geophysical models that can be used to calculate its effect are rare.

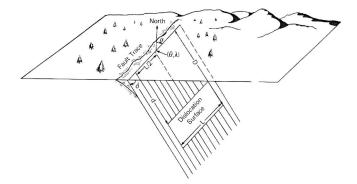
The final deformation field associated with the earthquake is the sum of the coseismic and postseismic components. Fig. 1 shows the coseismic (especially noticeable as the step function in the north coordinate) and postseismic (the long asymptotic tail following the step function) deformation as revealed by time series of positional coordinates for the continuously operating reference station (CORS) known as FAIR for a time period including the 2002 Denali earthquake. This earthquake is the largest that occurred within the United States since the CORS network was established. HTDP 3.0 contains models for 29 earthquakes (see Table 1) which have been developed from measured deformation on the Earth's surface. Locations range from Alaska to the Mexican border, although all but two are located in California. At this

**Table 1.** List of Earthquakes Having Models in HTDP 3.0

Earthquake	Date	Magnitude	Number of dislocations
Parkfield, Calif.	1934	6.0	98
El Centro, Calif.	1940	6.7	5
Red Mountain, Calif.	1941	5.9	1
San Jacinto, Calif.	1942	6.5	1
Kern County, Calif.	1952	7.7	3
San Jacinto, Calif.	1954	6.2	1
Prince Wm. Sound, Alaska	1964	9.2	68
Parkfield, Calif.	1966	5.6	98
Borrego Mtn, Calif.	1968	6.4	1
San Fernando, Calif.	1971	6.4	4
Imperial Valley, Calif.	1979	6.6	1
Coyote Lake, Calif.	1979	5.9	1
Homestead Valley, Calif.	1979	5.6	1
Coalinga, Calif.	1983	6.5	1
Morgan Hill, Calif.	1984	6.2	1
Kettleman Hills, Calif.	1985	6.1	1
Chalfant Valley, Calif.	1986	6.5	2
North Palm Springs, Calif.	1986	6.0	1
Superstition Hill, Calif.	1987	6.6	2
Whittier Narrows, Calif.	1987	6.0	1
Loma Prieta, Calif.	1989	7.1	1
Petrolia, Calif.	1992	7.1	1
Landers/Big Bear, Calif.	1992	7.3	26
Joshua Tree, Calif.	1992	6.1	19
Northridge, Calif.	1994	6.6	1
Hector Mine, Calif.	1999	7.1	75
San Simeon, Calif.	2003	6.5	200
Parkfield, Calif.	2004	6.0	300
Denali, Alaska	2002	7.9	911

time, only the coseismic deformations associated with the earth-quakes listed in Table 1 are modeled in HTDP. There are two other earthquakes with magnitudes greater than 6.2 that occurred in CONUS since 1980 that are not included in HTDP. These are the M 7.3 Borah Peak, Idaho earthquake which occurred in 1983 and the M 6.7 Nisqually, Washington earthquake which occurred in 2001. We do not intend to include a model of the 1983 Borah Peak earthquake because it predates the era of GPS surveys and NGS has decided to discontinue support for including classical surveys in future readjustments (Pearson 2005). We hope to include a model of the 2001 M 6.7 Nisqually, Washington earthquake in a future version of HTDP.

Another (third) type of slow, time-dependent motion that has been observed in the western U.S. is called a *slow-slip event*. These events produce surface displacements that appear very much like earthquakes but occur over weeks rather than seconds. They are similar to postseismic motions in that they do not produce seismic shaking but differ in that they are isolated in time rather than following a seismic event. Unlike secular velocities they are limited in duration. Such slow slip events have been observed along the coastal regions of Oregon and Washington (Dragert et al. 2004; Szeliga et al. 2008) and along the San Andreas fault in central California (Linde et al. 1996). Since the surface displacements observed to date from these events have been small (<5 mm), they are not specifically modeled in HTDP 3.0.



**Fig. 2.** Schematic diagram of a dislocation. The rectangle represents the dislocation surface or slipping patch on a fault. The deformation measured on the surface depends on the strike  $(\alpha)$  and dip  $(\delta)$  of the fault plane, the length of the dislocation (L), the depth to the top (d) and bottom (D) surface of the dislocation measured along the fault plane and the latitude and longitude  $(\theta)$  and  $(\theta)$  of the fault center.

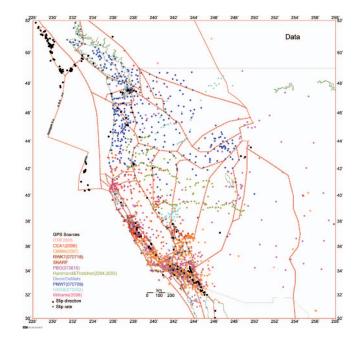
# **Dislocation Models**

Predicting the effect of an earthquake on positional coordinates utilizes the relatively simple mathematical equations provided by dislocation theory (Okada 1985; Savage 1980). The equations predict the elastic response of a uniform elastic half-space to slip on a rectangular patch embedded within the half-space. Each dislocation represents a rectangular patch (fault surface) in the Earth where one side slips relative to the other in the plane by a uniform amount. The name, dislocation, is used because the slip displacement is uniform over the rectangle thereby producing a discontinuity along the edges of the patch. The model is shown conceptually in Fig. 2. A dislocation model is thought to be similar to what happens during an earthquake where one side of the fault slips relative to the other. While a single dislocation can be used to model an earthquake, real earthquakes are much more complex. This oversimplification can be overcome by partitioning the fault into a series of smaller rectangular dislocations which, taken together, may better approximate the complexity associated with a real earthquake. In the Denali earthquake discussed below, for example, over 900 dislocations were used to map the fault plane.

The dislocations used in HTDP 3.0 were determined by varying the properties of the dislocations, such as the amount of slip and the geometry of the rectangular patches, until the predictions of the dislocation model provides a satisfactory match with observations made before and after the earthquake. The two main types of observations used to constrain dislocation models are surface measurements of displacements measured with GPS data and, sometimes, InSAR (Interferometric Synthetic Aperture Radar) data (Bürgmann et al. 2000).

### **Updated Model of the Secular Velocity Field**

The updated model of the secular field started with an analytical model representing horizontal crustal motion developed using the computer code DEFNODE (McCaffrey 1995, 2002) which incorporates all major active faults located in western CONUS in a single model developed by combining studies by McCaffrey (2005) of the Pacific northwest and McCaffrey et al. (2007) of the southwestern United States. The blocks included in the model are shown in Fig. 3.



**Fig. 3.** (Color) Tectonic blocks used to model secular motion. Lines outline the boundaries of the tectonic blocks used to model the data. The ITRF2005 velocity measurements and geological data used to constrain the secular velocity model incorporated into HTDP 3.0 are also shown.

The predicted velocity field is based on rotating, fault-bounded crustal blocks (spherical caps) subject to elastic and anelastic strain rates. Rotations of the blocks are described by angular velocities, sometimes called Euler poles. The angular velocity is constrained to have the center of the Earth as its origin, forcing the plates to move tangentially to the surface. Hence the plates have only east and north velocities due to rotations.

Elastic strain rates arise where the edges of the blocks (the faults) come into contact at a frictional surface. As the blocks slide past one another, frictional forces cause the shallow parts of the faults to remain stuck and this induces strain in the blocks adjacent to the fault. The amount of strain is estimated from the relative velocities of the blocks across the fault and the degree of locking (that varies from zero to one where zero corresponds to free slip and one corresponds to a fully locked fault). These parameters are passed through a dislocation model (as described earlier) but in a "back-slip" mode, or negative earthquakes, described by Savage (1983). The linear combination of the rotational motions and the back-slip velocities gives the appearance of the motion about a locked fault.

The model also allows the blocks to deform under horizontal, uniform strain rates. This allows for the distributed deformation associated with minor, unmodeled faults within the blocks that are often found in tectonically active areas. The uniform strain rates are implemented using the spherical-coordinate strain tensor of Savage et al. (2001).

We used this model to invert or solve for parameters that control the surface velocities. In the inversion, the free parameters are related to the blocks, the faults, and the GPS velocity fields. Each block has three free parameters describing the x, y, and z components of its angular velocity and three describing the EE, NN, and EN components of its uniform strain rate tensor. The parameterization of locking on the faults is through a parameter  $\varphi$  which is defined as one minus the free slip fraction. Hence,  $\varphi = 1$  represents

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Table 2. Geodetically Derived Velocity Vectors Used to Constrain the Secular Velocity Model in HTDP 3.0

Code	Number used	Number total	Weight factor	Sig min (mm/year)	Sig max (mm/year)	NRMS	WRMS (mm/year)	Sum of weights	Data source
ITR5	55	290	0.44	0.5	3.0	1.23	0.66	377	Altamimi et al. (2007)
SNRF	18	22	1.00	0.3	3.0	1.12	0.43	246	Stable North American Reference Frame Working Group (2007)
DXB2	16	16	1.00	0.3	5.0	0.67	0.85	20	Dixon et al. (2002)
HT04	67	67	1.00	0.5	3.0	0.90	0.86	146	Hammond and Thatcher (2004)
HT05	94	110	1.00	0.5	3.0	0.87	1.01	139	Hammond and Thatcher (2005)
WILL	36	71	0.25	0.5	3.0	1.19	1.14	78	Williams et al. (2006)
CEA1	1,285	1,403	1.00	0.3	2.5	1.21	1.33	2,150	California Earthquake Authority
CMM4	1,195	1,318	1.00	0.3	2.5	1.15	1.22	2,130	Z. K. Shen et al. ("A unified analysis of crustal motion in California 1970–2004," <i>The SCES Crustal Motion Map</i> , unpublished, 2007)
DMEX	12	14	0.44	0.5	3.0	0.75	1.07	12	Márquez-Azúa and DeMets (2003)
PBO7	437	795	0.25	0.4	3.0	1.07	0.95	1,100	PBO 4/2007
PNW7	578	670	1.00	0.3	2.5	1.16	0.58	4,590	McCaffrey et al. (2007); Payne et al. (2007)

full locking on the fault (no slip at the boundary) and  $\varphi$ =0 represents a free slip boundary at the fault. For short faults, a single value of  $\varphi$  is used along its entire length while longer faults may have  $\varphi$  changing along strike. The amount of back-slip applied at a point along the fault is  $-\varphi V$  where V is the slip vector locally on the fault. Finally, the GPS-derived velocities used to constrain the model parameters come from several individual publications, where the set of velocities from one publication may be referred to a different reference frame than the set from another publication. Hence, each set of vectors was transformed into ITRF2005 by applying three rotation parameters whose values were estimated along with the other parameters involved in our model. This estimation problem is highly nonlinear and was solved iteratively by the downhill simplex method.

The general geometry of the model has been described by McCaffrey (2005) for the southern part of the North American-Pacific plate boundary and McCaffrey et al. (2007) for the northern part. In this work, the two models were merged by modifying the block geometries at their common boundary along the latitude of the northern California border. Blocks included in the inversion process are shown in Fig. 3.

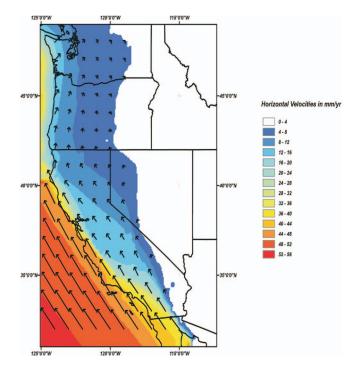
The model is constrained by the following data: 4,890 horizontal velocity vectors (derived from repeated geodetic observations—mostly GPS observations), 170 fault slip rates from geologic studies, and 258 fault slip vectors taken from earthquakes and geologic studies. The distribution of geodetically derived velocity measurements are shown in Fig. 3 and details of the various geodetic data sets are summarized in Table 2. Note that only horizontal velocities were used in the inversion.

Using these data, the model parameters were adjusted iteratively to produce an improved match to the weighted data. The fitness criterion was the reduced chi-square statistic; in the end this was 1.38 indicating that the data are fit at about their level of uncertainty. In Table 2, the normalized RMS (NRMS) indicates the degree of fit to the particular velocity field; a value of around unity indicates an acceptable fit. The weighted RMS (WRMS) is a measure of the weighted average residual for that field; for the majority these are about 1 mm/year or less.

Note that the data sets contained in Table 2 may have originally been expressed in various reference frames. Hence, as part of the DEFNODE process, the ITR5 velocity field was selected to define the reference frame and the velocity vectors contained in each of the other data sets were transformed into that frame. We

selected the data set called ITR5, because its vectors are expressed in the rigorously defined ITRF2005 frame (Altamimi et al. 2007). Consequently, HTDP 3.0 predicts velocities relative to ITRF2005, but the software is able to convert these predicted ITRF2005 velocities to other popular reference frames, including NAD 83 (CORS96). Fig. 4 displays predicted secular velocities in western CONUS relative to NAD 83 (CORS96).

Once model parameters have been estimated with DEFNODE, these parameters can be used to predict the horizontal velocity at any point in western CONUS by running DEFNODE in its predictive (forward model) mode. HTDP uses four grid files to interpolate the secular velocities predicted by DEFNODE. These grids cover different regions with different cell sizes in order to maintain a desired level of accuracy in regions of higher velocity gra-



**Fig. 4.** (Color) Horizontal velocities in western CONUS relative to NAD 83 (CORS96) as predicted with HTDP 3.0. Colors indicate velocity magnitudes and arrows indicate velocity directions.

**Table 3.** Interpolation Grids Incorporated into HTDP 3.0

Longitude range	Latitude range	Cell spacing (min)	Grid dimensions	Region
125° to 100°W	31°-49°N	15	101×73	Entire region
125° to 122°W	$40^{\circ} - 49^{\circ} N$	3.75	$49 \times 145$	Pacific NW
125° to 119°W	36°-40°N	3.75	$97 \times 65$	Northern California
121° to 114°W	31°-36°N	3.75	113×81	Southern California

dients. HTDP will automatically choose the most accurate grid for the point in question. The grids are summarized in Table 3. Note that HTDP is now capable of estimating secular velocities over the region from 31° to 49°N latitude and from 125° to 100°W longitude, which is significantly larger than the previous version which extended from 31.75° to 50°N latitude and from 125° to 111°W longitude.

For a point located on that part of the North American plate which resides external to the interpolation grids (presumably "stable" North America), HTDP 3.0 uses the Euler pole for North America, which was derived by Altamimi et al. (2007), to predict the point's ITRF2005 velocity. It should be noted that when the ITRF2005 velocity for such a point is transformed to its corresponding NAD 83 (CORS96) velocity, then the resulting velocity usually differs from zero. Hence, HTDP 3.0 predicts small but nonzero NAD 83 horizontal and vertical velocities for points located in stable North America for two reasons, both related to deficiencies in the definition of NAD83: first, because the velocity-related parameters included in the transformation from ITRF96 are based on the NUVEL1A-NNR plate motion model (DeMets et al. 1990, 1994) rather than the plate motion model associated with ITRF2005; and second, because the ITRF2005 reference frame is moving relative to the ITRF96 reference frame. To rectify this problem, NGS is considering the possibility of introducing a more modern realization of NAD 83 within the next few years, after the next ITRF realization is released. This modern NAD 83 realization would be directly linked to this next ITRF realization rather than indirectly linked to it via a relationship with ITRF96. The new relationship between NAD 83 and ITRF would also be based on the prevailing plate motion model existing at the time when the new NAD 83 realization is formulated. That is, the new relationship between NAD 83 and ITRF would be based on the prevailing estimates for the parameters that quantify the Euler Pole for the North American plate relative to the new ITRF realization. Note that the same datum transformation can cause HTDP to predict small vertical velocities in the NAD83 reference frame when interpolating from our velocity grids even though the gridded velocities, which are in ITRF2005, have zero vertical velocities. This affects only HTDP3.0. In previous versions (HTDP2.9 and earlier) velocities for the grid nodes are referred to NAD 83 (CORS96).

"Observed" velocity vectors for seven small regions were excluded from the inversion because these regions contain geophysical features such as volcanoes or the epicentral region of large recent earthquakes where the deformation is not easily modeled using the methodology described above. These regions are described by the coordinates (latitude and longitude) of the region's center and a radius. The regions are listed in Table 4 below. Users should be aware of these regions because the predicted velocities and thus the corrections applied to positions and survey measurements may be less accurate there than elsewhere in the study area.

### Validation of Secular Field

The predicted secular velocity field contained in HTDP 3.0 was tested by comparing it to two GPS-derived data sets. The first data set was the GPS vectors used to develop the model. Here we were simply checking to see that the grids in HTDP accurately represent the velocity field. The agreement (summarized in Table 5) was generally very good. The RMS residuals for 4,890 vectors were 0.75 mm/year in the north component and 0.68 mm/year in the east component. The maximum residuals were a little over 10 mm/year in both the north and east components; however the 13 residuals with a combined vector greater than 5 mm/year fall within a narrow linear concentration that seems to follow the San Andreas Fault system through California with about half distributed along the creeping segment of the San Andreas Fault (Thatcher et al. 1997). A poor fit in this area is not unexpected because the interpolation procedure used by HTDP cannot be expected to follow the very high strain gradients associated with the creeping fault. Histograms of the residuals are shown in Figs. 5(a and b).

The second test data set used to validate the secular field for HTDP 3.0 was the velocities estimated by the California Spatial Reference Center using the "Scripps Epoch Coordinate Tool and Online Resource" (SECTOR) (Nikolaides 2002). The velocities we used are available at: http://sopac.ucsd.edu/cgi-bin/rerunTimeSeries.cgi. While some of the stations in this data set are also used to develop the model, the data were independently processed and the SECTOR utility for determining the velocities

**Table 4.** Circular Regions Excluded from the Inversion

		Center latitude			Center longitude		
Name	Degrees	Minutes	Seconds	Degrees	Minutes	Seconds	Radius (km)
Mammoth lakes volcanic region	37	42	0	118	54	0	20
Coso volcanic field	36	0	0	117	45	0	20
Yellowstone volcanic region	44	25	48	110	40	12	50
South sister volcano	44	6	0	121	51	0	20
Mount St. Helens volcano	46	12	0	122	10	48	20
Landers quake	34	24	-0	116	30	0	20
Landers quake	34	0	0	116	30	0	20

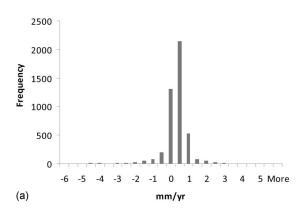
**Table 5.** Summary of Data Sets Used to Test HTDP 3.0

Data set	RMS north residual (mm/year)	RMS east residual (mm/year)	Number of vectors	
Inversion data	0.75	0.68	4558	
Sector in HTDP30	1.9	1.7	630	
Sector in HTDP29	3.3	3.1	630	

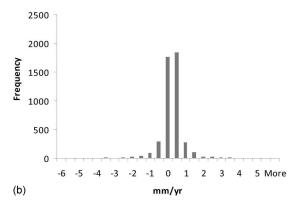
is very different from the method used by the inversion. In addition, they included up to two years of additional measurements. For these reasons it is believed that velocity estimates for the common stations are independent. Initially the comparison produced a large number of outliers, however, most of these proved to be cases with short time series and these disappeared once test data sets were restricted to stations with a minimum of 2 years of data.

The fit of these data was excellent (see Table 5) with the RMS residuals being 1.9 mm/year for the north and 1.7 mm/year for the east components. Over 90% of the stations had a combined residual of less than 3 mm/year. Histograms of the residuals are shown in Figs. 6(a and b) and a map of points with total residuals greater than 5 mm/year is shown in Fig. 7. By way of comparison, using the same data set, HTDP 2.9 has RMS residuals of 3.3 mm/year for the north and 3.1 mm/year for the east component. So introducing the new model of the secular field produces a

# **North Residual**

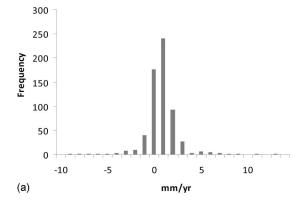


# **East Residual**

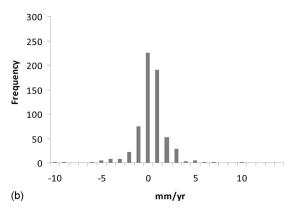


**Fig. 5.** (a) Histogram of north component residuals of GPS vectors included in inversion; (b) histogram of east component residuals

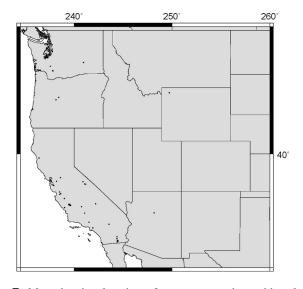
# **North Residual**



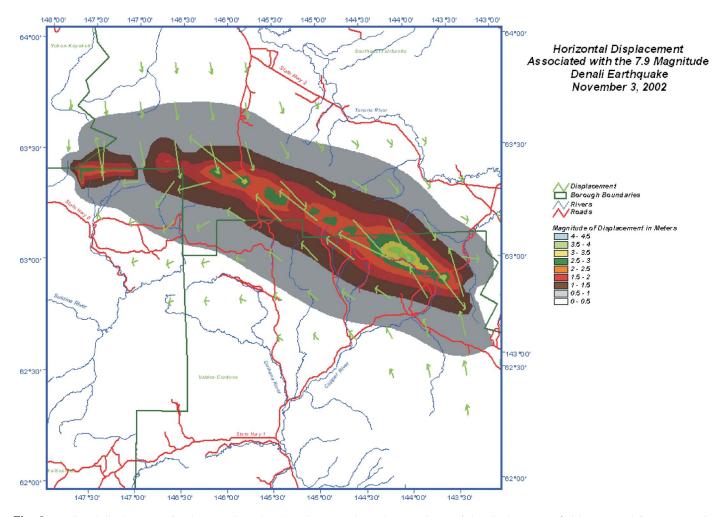
# **East Residual**



**Fig. 6.** (a) Histogram of *N* component residuals for SECTOR derived velocities; (b) histogram of east component residuals for SECTOR derived velocities



**Fig. 7.** Map showing location of sector test points with velocity residuals exceeding 5 mm/year in magnitude



**Fig. 8.** Predicted displacement for the Denali earthquake. Contours show the magnitude of the displacements (without regard for the opposite direction of the displacement on different sides of the fault) and arrows show predicted directions of the displacements.

significant (over 30%) improvement in the fit to the observed velocities from the SECTOR utility.

# Denali Earthquake

The Denali earthquake occurred on Sunday, November 3, 2002 at 22:12 UTC in south central Alaska about 283 km NNE of Anchorage. The earthquake had a magnitude (Mw) of 7.9 and was the strongest ever recorded in the interior of Alaska and one of the largest earthquakes recorded within the United States (Eberhart-Phillips et al. 2003). The earthquake produced displacements of several meters near the fault and measurable displacements throughout most of central Alaska. Because this earthquake was primarily a strike-slip event where the rupture plane extended to the surface, points on opposite sides of the fault will move in opposite directions producing a very large relative displacement for a pair of points that happen to be located on opposite sides of the fault. The earthquake was predominantly a right-lateral strikeslip event; however, it started with a thrust subevent on the previously unrecognized Susitna Glacier fault. The dislocation model we used for this earthquake was developed by Elliott et al. (2007), which was constrained by surface deformation measurements (both GPS data and range offsets derived from a synthetic aperture radar (SAR) amplitude image) without using seismic body waves. Because of the complexity of this event, combined with the fact that the rupture extended over 250 km along the Denali fault, the dislocation model used to model this earthquake, with 910 elements, was the most complex ever incorporated in HTDP. Indeed the number of dislocation elements in this model is more than three times any of the other dislocation models included in the software. The predicted displacements for the Denali earthquake are shown in Fig. 8.

The predicted movement associated with the Denali earth-quake was tested using a set of over 200 GPS-derived displacement vectors. The agreement between predicted and observed displacements was reasonably good with an RMS misfit of 0.1 m in both the north and east components. A few quite large discrepancies (sometimes >1 m) were found in the vicinity of the fault trace. This probably indicates that complex fault geometry can introduce significant errors in the predicted deformation for points located near the rupture plane. This is particularly true for large earthquakes that rupture the Earth's surface. As a result, care must be used when correcting surveys for earthquakes when the survey area crosses a fault rupture that extends to the Earth's surface. As shown in Fig. 1 we also compared the HTDP 3.0 predicted displacement for this earthquake for the CORS station FAIR with the time series from this station covering the time of the earthquake.

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#### **Future Plans**

The major deficiency with HTDP 3.0 is the lack of a detailed crustal motion models for Alaska. Currently the HTDP 3.0 model includes models for only the Prince William Sound earthquake of 1964 and the Denali earthquake of 2002, and the model for the secular velocity field has not been updated. Over the next year or so, HTDP may be revised to include a model of recent major (greater than magnitude 7) earthquakes and an improved model for Alaska's secular velocity field.

### **Conclusions**

The HTDP software has been updated to include a new model of the secular velocity field in western CONUS and a model of the Denali earthquake of 2002. The model was released in June 2008 replacing the previous version, HTDP 2.9 (Pearson and Snay 2007), which had been used in the recently completed NSRS2007 readjustment (Pearson 2005). HTDP 3.0 is applied in all OPUS solutions to convert computed NAD 83 coordinates from the day when the submitted GPS data was observed to a common reference date of January 1, 2002. The HTDP 3.0 software is also available for download at http://www.ngs.noaa.gov/PC\_PROD/HTDP/. Finally, the latest version of HTDP can be run interactively on the Web at http://www.ngs.noaa.gov/TOOLS/Htdp/Htdp.shtml.

With its new secular velocity field model, HTDP is now capable of predicting secular velocities over the region from 31° to 49°N latitude and from 125° to 100°W longitude. This is significantly larger than the region covered by the previous version of HTDP. The model also includes three subgrids with reduced cell spacing that allows HTDP to obtain higher accuracy in regions of higher velocity gradients in the tectonically active areas of California and the Pacific Northwest. A test of the secular field model versus an extensive data set compiled by the California Spatial Reference Center showed that the new model of the secular velocity field produces a significant (over 30%) improvement in the fit to the observed velocities as compared to the model incorporated in HTDP 2.9 and previous versions.

Tests of the 2002 Denali earthquake showed that points located in the vicinity of the fault trace sometimes had quite large residuals. This probably indicates large earthquakes that break the Earth's surface can be difficult to model accurately in the area near the ruptured surface. This shows why care must be used when correcting geodetic data for earthquakes in the vicinity of a ruptured surface fault.

# **Acknowledgments**

We thank the California Spatial Reference Center, particularly Peng Fang, Yehuda Bock, Linette Prawirodirdjo and Paul Jamason, for making data from the SECTOR utility available for validating the secular velocity field contained in HTDP 3.0. We also thank Cindy Craig of NGS for providing the maps shown in Figs. 4 and 8.

# Appendix. Transforming Coordinates between ITRF2005 and NAD 83

This Appendix presents the NGS-adopted equations for transforming positional coordinates between ITRF2005 and NAD 83

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(CORS96). These equations have been incorporated into version 2.9 of HTDP, as well as into version 3.0. The name, NAD 83 (CORS96), will be truncated to NAD 83 here to simplify the text.

Let  $x(t)_{\text{NAD }83}$ ,  $y(t)_{\text{NAD }83}$  and  $z(t)_{\text{NAD }83}$  denote the NAD 83 positional coordinates for a point at time t as expressed in a 3D Cartesian Earth-centered, Earth-fixed coordinate system. These coordinates are expressed as a function of time to reflect the reality of the crustal motion associated with plate tectonics, land subsidence, volcanic activity, postglacial rebound and so on. Similarly, let  $x(t)_{\text{ITRF}}$ ,  $y(t)_{\text{ITRF}}$ , and  $z(t)_{\text{ITRF}}$  denote the ITRF2005 positional coordinates for this same point at time t. The given ITRF2005 coordinates are related to their corresponding NAD 83 coordinates by a time-dependent transformation that is approximated by the following equations:

$$x(t)_{\text{NAD 83}} = T_x(t) + [1 + s(t)] \cdot x(t)_{\text{ITRF}} + \omega_z(t) \cdot y(t)_{\text{ITRF}}$$

$$- \omega_y(t) \cdot z(t)_{\text{ITRF}}$$

$$y(t)_{\text{NAD 83}} = T_y(t) - \omega_z(t) \cdot x(t)_{\text{ITRF}} + [1 + s(t)] \cdot y(t)_{\text{ITRF}}$$

$$+ \omega_x(t) \cdot z(t)_{\text{ITRF}}$$

$$z(t)_{\text{NAD 83}} = T_z(t) + \omega_y(t) \cdot x(t)_{\text{ITRF}} - \omega_x(t) \cdot y(t)_{\text{ITRF}}$$

$$+ [1 + s(t)] \cdot z(t)_{\text{ITRF}}$$

$$(1)$$

Here,  $T_x(t)$ ,  $T_y(t)$ , and  $T_z(t)$ =translations along the x, y, and z axes, respectively;  $\omega_x(t)$ ,  $\omega_y(t)$ , and  $\omega_z(t)$ =counterclockwise rotations about these same three axes; and s(t)=differential scale change between ITRF2005 and NAD 83. These approximate equations suffice because the three rotations have small magnitudes. Note that each of the seven quantities is represented as a function of time because space-based geodetic techniques have enabled scientists to detect their time-related variations with some degree of accuracy. These time-related variations are assumed to be mostly linear, so that the quantities may be expressed by the following equations:

$$T_{x}(t) = T_{x}(t_{0}) + T'_{x} \cdot (t - t_{0})$$

$$T_{y}(t) = T_{y}(t_{0}) + T'_{y} \cdot (t - t_{0})$$

$$T_{z}(t) = T_{z}(t_{0}) + T'_{z} \cdot (t - t_{0})$$

$$\omega_{x}(t) = \left[\varepsilon_{x}(t_{0}) + \varepsilon'_{x} \cdot (t - t_{0})\right] \cdot m_{r}$$

$$\omega_{y}(t) = \left[\varepsilon_{y}(t_{0}) + \varepsilon'_{y} \cdot (t - t_{0})\right] \cdot m_{r}$$

$$\omega_{z}(t) = \left[\varepsilon_{z}(t_{0}) + \varepsilon'_{z} \cdot (t - t_{0})\right] \cdot m_{r}$$

$$s(t) = s(t_{0}) + s' \cdot (t - t_{0})$$
(2)

where  $m_r$ =4.848 136 81·10<sup>-9</sup>=conversion factor from milliarc seconds (mas) to radians.

Here,  $t_0$  denotes a fixed, prespecified time of reference. Hence the seven quantities  $T_x(t_0)$ ,  $T_y(t_0)$ ,...,  $s(t_0)$  are all constants. The seven other quantities:  $T_x'$ ,  $T_y'$ ,..., s', which represents rates of change with respect to time, are also assumed to be constants.

The transformation from ITRF2005 to NAD 83, denoted (ITRF2005  $\rightarrow$  NAD 83) is defined in terms of the composition of two distinct transformations, applied sequentially. First, positional coordinates are transformed from ITRF2005 to ITRF2000, then from ITRF2000 to NAD 83. This composition may be symbolically expressed via the following equation:

**Table 6.** Transformation Parameters

Parameter	Units	(ITRF2005 $\rightarrow$ ITRF2000) $t_0 = 2,000.00$	(ITRF2005 $\rightarrow$ ITRF2000) $t_0 = 1,997.00$	(ITRF2000 $\rightarrow$ NAD 83) $t_0 = 1,997.00$	(ITRF05 $\to$ NAD 83) $t_0 = 1,997.00$
$T_x(t_0)$	Meters	+0.0001	+0.0007	+0.9956	+0.9963
$T_{v}(t_0)$	Meters	-0.0008	-0.0011	-1.9013	-1.9024
$T_z(t_0)$	Meters	-0.0058	-0.0004	-0.5215	-0.5219
$\varepsilon_{x}(t_{0})$	mas	0.000	0.000	+25.915	+25.915
$\varepsilon_{y}(t_{0})$	mas	0.000	0.000	+9.426	+9.426
$\varepsilon_z(t_0)$	mas	0.000	0.000	+11.599	+11.599
$s(t_0)$	ppb	+0.40	+0.16	+0.62	+0.78
$T_x'$	m/year	-0.0002	-0.0002	+0.0007	+0.0005
$T'_{y}$	m/year	+0.0001	+0.0001	-0.0007	-0.0006
$T_z'$	m/year	-0.0018	-0.0018	+0.0005	-0.0013
$\varepsilon_x^{'}$	mas/year	0.000	0.000	+0.067	+0.067
$\varepsilon_y^{'}$	mas/year	0.000	0.000	-0.757	-0.757
$oldsymbol{arepsilon_z'}$	mas/year	0.000	0.000	-0.051	-0.051
s'	ppb/year	+0.08	+0.08	-0.18	-0.10

Note: Counterclockwise rotation of axes are positive; mas=milliarc second; and ppb=parts per billion.

$$(ITRF2005 \rightarrow NAD 83) = (ITRF2005 \rightarrow ITRF2000)$$
$$+ (ITRF2000 \rightarrow NAD 83)$$
(3)

where (ITRF2005  $\rightarrow$  ITRF2000) denotes the transformation from ITRF2005 to ITRF2000, and (ITRF2000  $\rightarrow$  NAD 83) denotes the transformation from ITRF2000 to NAD 83. For (ITRF2005  $\rightarrow$  ITRF2000), HTDP uses the parameter values adopted by the International Earth Rotation and Reference System Service (IERS) for  $t_0$ =2,000.00 (=1 January 2000) (see Altamimi et al. 2007). Natural Resources Canada has also adopted the IERS ITRF2005  $\rightarrow$  ITRF2000 transformation in deriving its official ITRF2005  $\rightarrow$  NAD 83 transformation [see Craymer (2006)]. We have converted the IERS-adopted values for  $t_0$ =2,000.00 to their corresponding values for  $t_0$ =1,997.00. Table 6 displays both sets of values.

For (ITRF2000 $\rightarrow$ NAD 83), HTDP uses the parameter values adopted both by Natural Resources Canada and NGS for  $t_0$  =1,997.00 (Soler and Snay 2004). Table 6 also displays these values. Because the values for the parameters associated with (ITRF2005 $\rightarrow$ ITRF2000) and with (ITRF2000 $\rightarrow$ NAD 83) are rather small in magnitude, the values for the parameters of (ITRF2005 $\rightarrow$ NAD 83) at  $t_0$ =1,997.00 may be computed with sufficient accuracy by adding the corresponding values for (ITRF2005 $\rightarrow$ ITRF2000) at  $t_0$ =1,997.00 with those for (ITRF2000 $\rightarrow$ NAD 83) at  $t_0$ =1,997.00. The right-most column of Table 6 displays the resulting values used by HTDP. The inverse transformation (NAD 83 $\rightarrow$ ITRF2005) at  $t_0$ =1,997.00 is obtained by changing the sign for each of the 14 values appearing in this column.

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